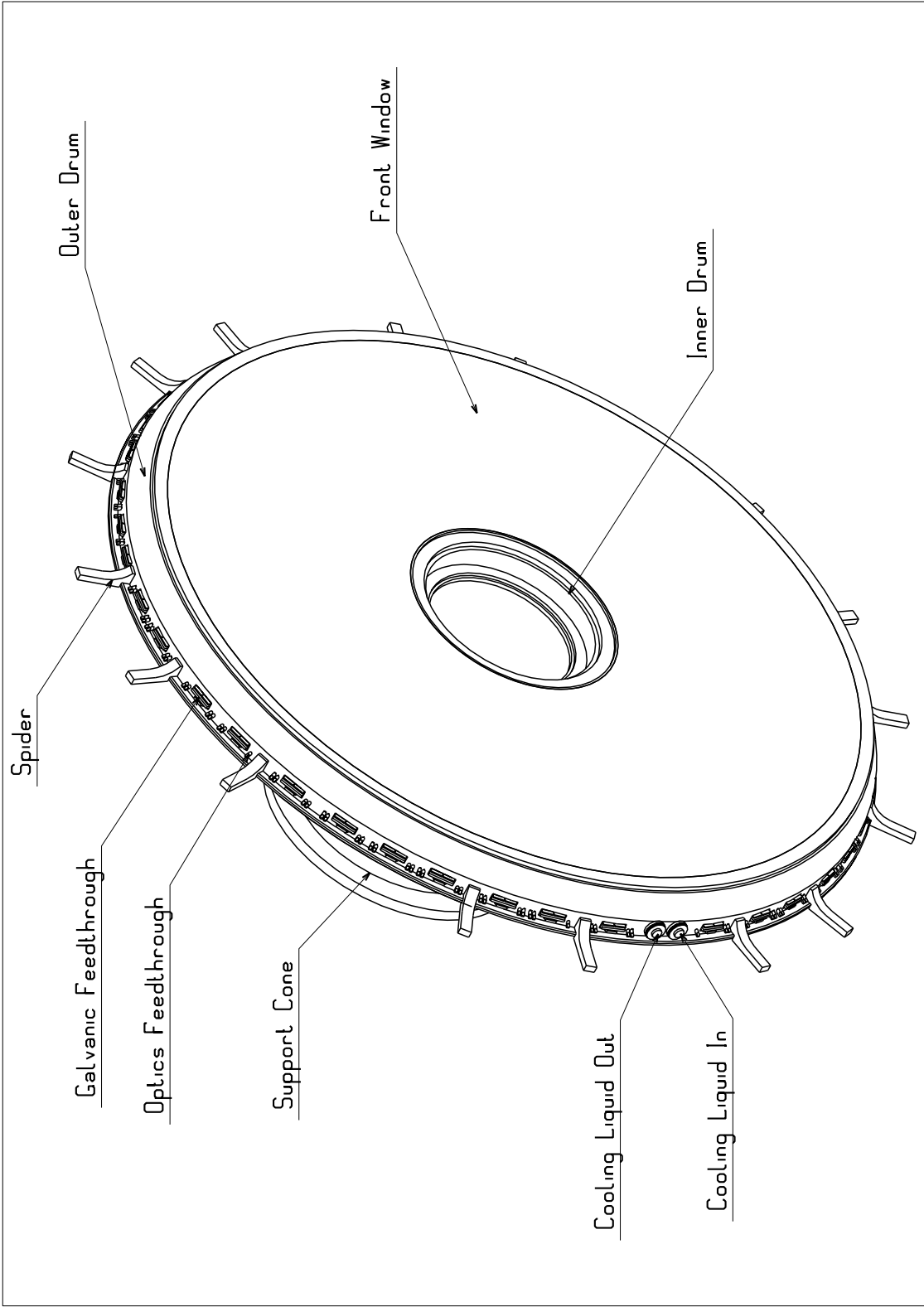


Status report on Preshower (SE) cooling

- on the Preshower and its cooling
- cooling needs and thermal inertia
- coolant transfer pipes on CMS Endcap :
 - * foam insulation, condensation, artificial heating
 - * pipe routing on Endcap
 - * cable chains



Preshower cooling in a nutshell

(detailed discussion : Review ECAL EDR-4)

- keep Si sensors cold enough (-5°C or lower)
- deal with dissipation of electronics
- SE detector (one on each endcap) has appearance of a freezer :
 - reasonably gas-tight containment
 - walls foam-insulated at the inside
 - container walls at $+18^{\circ}\text{C}$ (controlled)
 - feedthroughs (looks like a cryostat !)
- cooled by 2x2 large-surface, flat cooling screens (Al , brazed)
- C_6F_{14} (liquid !) ; needed SE entrance temp. = -15°C
- typical (turbulent) conditions inside cooling screens ($Re \sim 6000$ $Nu \sim 70$)
- no manifolding outside the freezer
- minimal amount of pipes connected to freezer : 2 inlets (just below beam level) and 2 outlets (just above beam) - see redundancy scheme of M. Jeske
- with this : safe behaviour in case of failure of 1 of the 2 circuits (power off)
- 0.9 ltr/s per pipe
- liquid warming up at SE exit : 2.6 degrees

Refrigeration power for SE (per endcap)

With 'pessimistic' scenarios :

* Dissipation : Si detectors, electronics, voltage regulators :

4 kW per read-out plane (x 2) -> **8 kW**

* Heat inleak through window foam : 0.75 kW (x 2) -> **1.5 kW**
(assumptions : 7 mm , 0.03 W/(m deg) , 18°C -> -14°C)

* Heat inleak through (galvanic) feedthrough station :

3.7 W (x 38) -> **0.14 kW**

* Heat inleak through (rest of) outer drum :

very rough estimate : -> **0.5 kW**

* Inner drum : neglected

* Dissipation in cables inside SE : unknown ; most probably not dominant

=> **total : about 10 kW per endcap**

SE tank thermal time constant

Capacitance of cold masses :

713 kg of Pb + 578 kg of Al

$C = (8.56 \cdot 10^4 + 5.18 \cdot 10^5) \text{ J/deg} = 6.04 \cdot 10^5 \text{ J/deg} = 0.17 \text{ kWh/deg}$

Conductances : per window : 23.6 W/deg (x 2)

feedthrough : 0.01 W/deg (x 38)

outer drum : 17 W/deg

total conductance = 68 W/deg

=> resistance $R = 15 \text{ deg/kW}$

Time constant $\tau = RC = \mathbf{2.5 \text{ hours}}$ (only !!!!!)

SE coolant transfer pipes : baseline

- pipe itself : austenitic stainless steel ; 32 mm OD ; 30 mm ID

=> $v = 1.25 \text{ m/s}$

=> specific pipe loss :

$$\frac{dp}{ds} \approx -10 \cdot \frac{\text{mbar}}{\text{m}}$$

=> loss per transition (take $\zeta = 1$) :

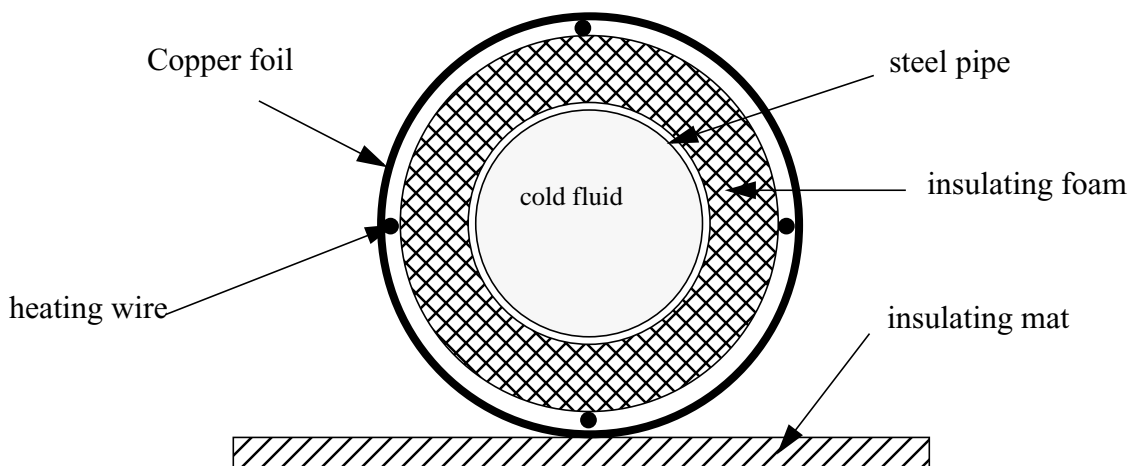
$$\Delta p_{trans} = \zeta \cdot \frac{\rho v^2}{2} = 14 \text{ mbar}$$

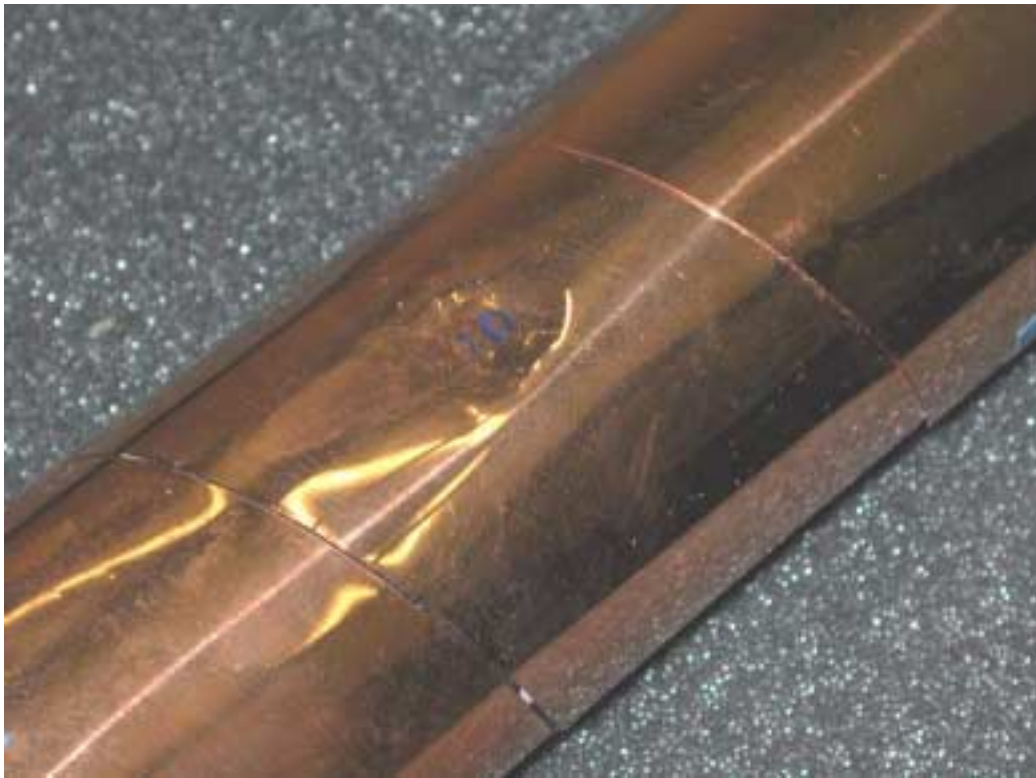
- design guidelines for (Armaflex AF grade) foam : thickness 21 mm necessary to avoid condensation => 74 mm OD over-all !

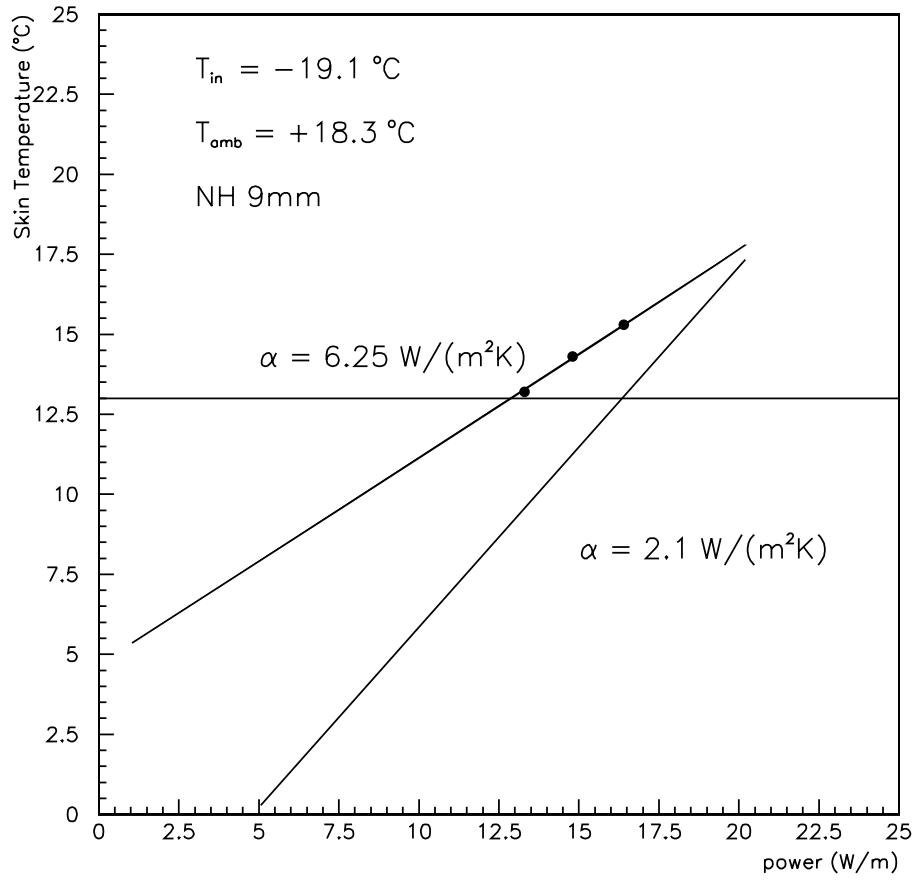
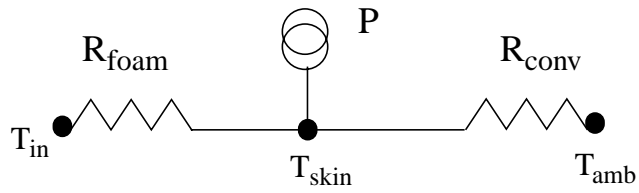
Problems :

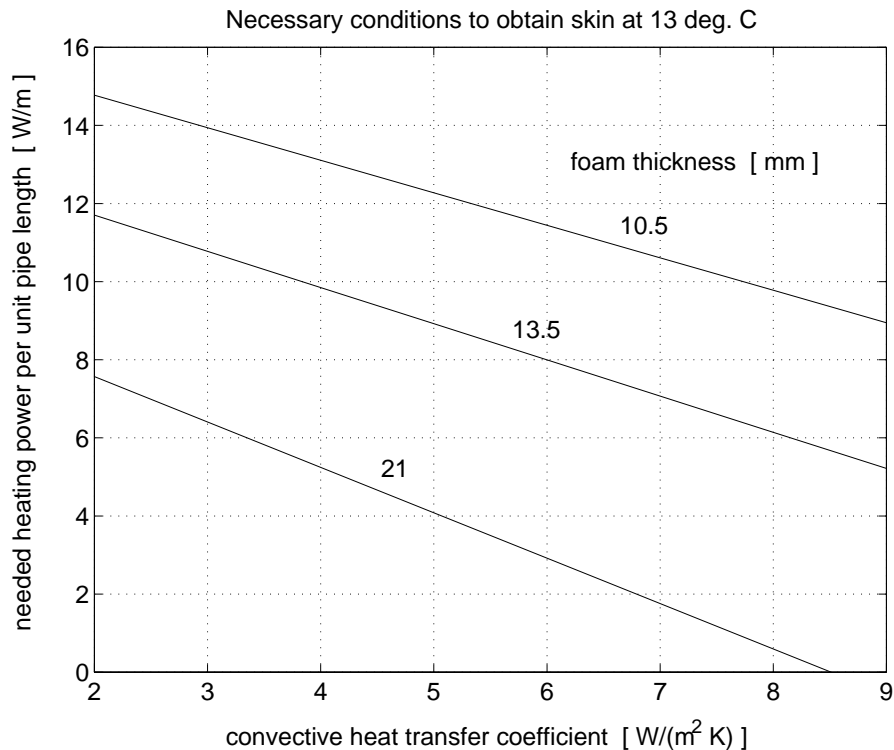
1. Foam grade : we think only AF is possible, but only NH allowed by TIS.
We may need to apply for a derogation.

2. Foam thickness : not everywhere is there space for 74 mm OD.
Wherever thickness has to be reduced, artificial heating is necessary
Dedicated testing work : reported upon in CMS IN 2001/036









What we intend to do :

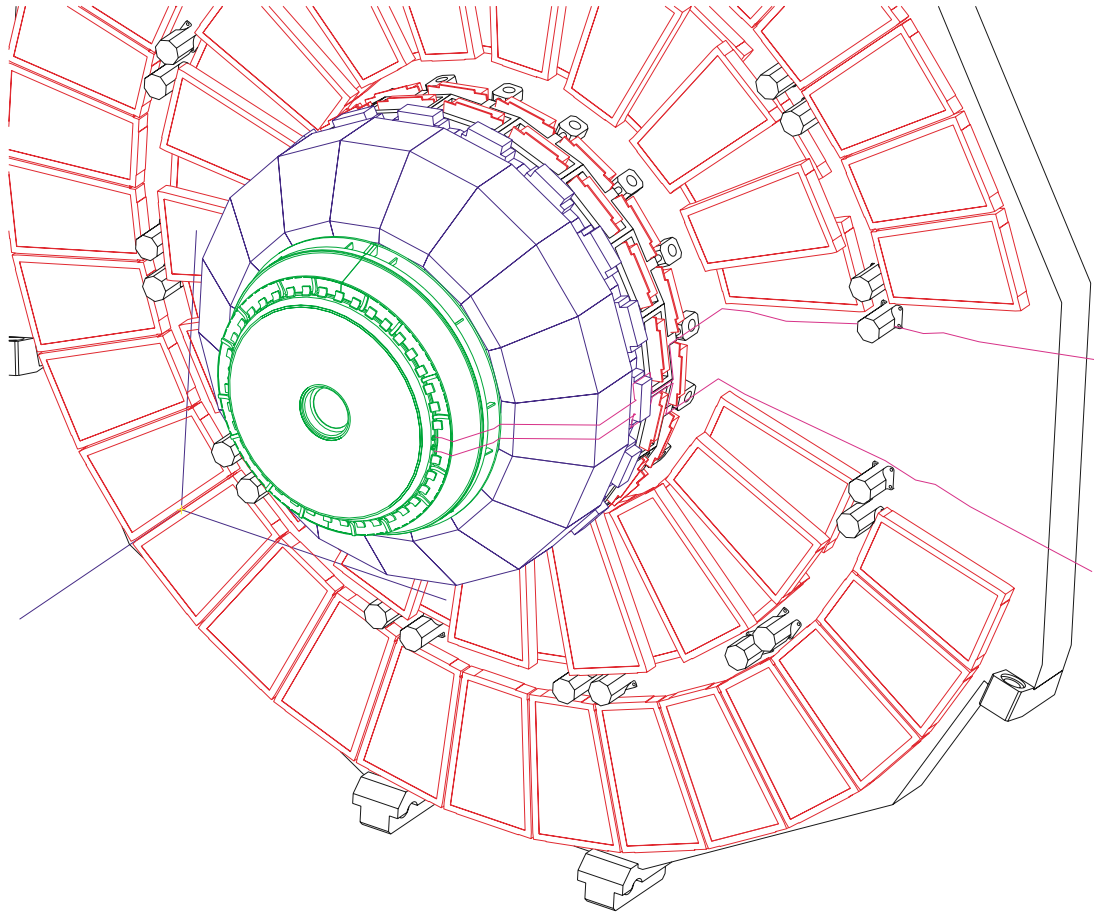
- design foam thickness wherever possible
- reduced foam thickness wherever required
- heating wires and Cu foil all along
- tune wire gage (resistance) to foam thickness
- the same 32/30 steel pipe all along except from 53° crack (see further)

3. Difficult pipe routing

From SE connection to CMS outside :

- avoid clash with TK support bracket
- allow EE to move in/out (with SE gone)
- in 53° crack : avoid HE connectors
- on cylindrical part of Endcap nose : avoid HE readout boxes
- buried behind ME/1/2 and ME/1/3
- no space for intermediate disconnections => **welded construction all along**

We try to replace the stiff pipe by a **DN32 flexible line in the 53° crack**, in order to free (transverse) space for EE motions. Reduced foam thickness (14.5 mm) resulting in over-all diam. ~ 72 mm . Trying to find Cu braid to put around foam.



SE coolant transfer through Endcap cable chains

Current baseline, under discussion with Integration :

- cryogenic transfer line (simplified , no superinsulation necessary)
- inner hose DN32
- over-all diameter ~ 90 mm